Fast generation and detection of spatial modes of light using an acousto-optic modulator

BORIS BRAVERMAN, 1,* D ALEXANDER SKERJANC, 1 D NICHOLAS SULLIVAN, 1 D AND ROBERT W. BOYD 1,2 D

Abstract: Spatial modes of light provide a high-dimensional space that can be used to encode both classical and quantum information. Current approaches for dynamically generating and measuring these modes are slow, due to the need to reconfigure a high-resolution phase mask such as a spatial light modulator or digital micromirror device. The process of updating the spatial mode of light can be greatly accelerated by multiplexing a set of static phase masks with a fast, image-preserving optical switch, such as an acousto-optic modulator (AOM). We experimentally realize this approach, using a double-pass AOM to generate one of five orbital angular momentum states with a switching rate of up to 500 kHz. We then apply this system to perform fast quantum state tomography of spatial modes of light in a 2-dimensional Hilbert space by projecting the unknown state onto six spatial modes comprising three mutually unbiased bases. We are able to reconstruct arbitrary states in under 1 ms with an average fidelity of 96.9%.

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Introduction

The application of spatial of modes of light to classical and quantum communication is an area of active research, because of the potential for increased energy efficiency and total data throughput [1–4]. One of the outstanding challenges to the practical application of spatial encoding is the slow rate at which distinct modes may be generated and detected. On the signal detection side, performing rapid and scalable spatial mode analysis is particularly desirable in the context of noisy and turbulent channels [5,6], since fast and complete channel characterization is necessary for adaptive-optic noise compensation in real time [7,8].

Several approaches to generating spatial modes have been previously demonstrated, but none attain an ideal combination of speed, efficiency, scalability, and reconfigurability. Actively and arbitrarily switchable spatial mode generation is currently performed with adaptive optics such as spatial light modulators (SLMs) or digital micromirror devices (DMDs) which alter the phase and amplitude front of the beam [9]. Both of these have refresh rates on the order of 1 kHz, which limits potential data transmission rates. This limitation is especially problematic for quantum key distribution (QKD) [10] where the mode must be updated before every transmitted photon to ensure communication security. An alternative approach is to use multiple electro-optical modulators (EOMs) to illuminate one of several static phase plates, and recombine the resulting spatial modes using several beamsplitters [1]. This method has the advantage of being very rapid (on the order of tens of GHz), but the efficiency of such a device scales as 1/N, where N is the number of desired modes. The mode conversion efficiency can be increased from $\sim 1/N$ to a fixed amount of loss by the use of multi-plane light conversion (MPLC) [11], where the desired spatial mode is generated through several reflections from a suitably patterned SLM. In order to produce different spatial modes at different times, MPLC would still require a number of switches

 $^{^{}I}$ Department of Physics and Max Planck Centre for Extreme and Quantum Photonics, University of Ottawa, 25 Templeton Street, Ottawa, ON, K1N 6N5, Canada

²Department of Physics and Astronomy, University of Rochester, 275 Hutchison Road, Rochester, NY 14627,

^{*}bbraverm@uottawa.ca

that scales as N. When N becomes large, these approaches can become prohibitively expensive, limiting their scalability.

An acousto-optical modulator (AOM) is a common device that can act as a rapid, high-efficiency optical deflector with good multi-mode performance. AOMs are often used to control the propagation direction of light, similarly to how one would use a steerable mirror, acting like an N-port switch and allowing much greater efficiency and scaling capabilities than an N-port beamsplitter array [12]. A double-pass AOM can be used to scan the frequency of a laser without affecting its spatial mode [13]. In this configuration, different RF frequencies applied to the AOM cause the output beam to be steered and re-focused on different regions of a retroreflection mirror, which can be seen as a folded 4-f optical system. AOMs are also used to synthesize arrays of rapidly movable focal spots for trapping atoms [14]. Most often the spatial structure of the beam remains Gaussian, just like the input beam, with dynamical control exerted only over the beam's position or propagation direction.

Replacing the mirror of a folded 4-f system with a hologram (as shown in Fig. 1) allows different spatial modes to be encoded onto the reflected light when the input beam is steered to different regions of the hologram. By imprinting a linear phase grating onto the hologram, we can separate the light with the imprinted spatial mode structure from the zeroth order reflection. Thus, we can generate nearly-pure spatial modes of light with a rate limited only by the modulation rate of the AOM, which can readily reach f = 1 MHz. When realizing the hologram using an SLM with a resolution on the order of 10^3 pixels, at least 10 modal patterns can be arranged side by side to select from N = 10 distinct (and arbitrary) modes.

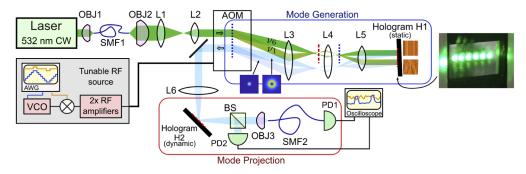


Fig. 1. Scheme for rapidly switching between different spatial modes of light by using an AOM as a rapidly steerable mirror to multiplex multiple regions of a static hologram (H1). The generated modes are then analyzed using mode projection with a dynamic hologram (H2) and an SMF. Both holograms are implemented using SLMs. The blue dotted lines show the positions of object planes (near-field) of the AOM, while red dotted lines indicate the positions of the image planes (far field) of the AOM (which are also the object planes for the SLMs). Abbreviations used in the figure: acousto-optic modulator (AOM); beam sampler (BS); objective lens (OBJ); photodiode (PD); single-mode fiber (SMF); voltage-controlled oscillator (VCO).

AOMs have been successfully used to steer light toward one of a set of fixed holograms to realize rapidly switchable spatial patterns of light, often in the context of real-time holographic displays [15,16] and synthesized aperture radar [17]. While these works have demonstrated high modulation and switching rates for the generated light patterns, the measurements were focused only on the intensity distribution of the light and not its phase profile. In the context of quantum optics and quantum communication [1–8], both the amplitude and phase of the spatial modes play a role in encoding information, and thus a full characterization of the complex field must be performed.

In most previous experiments, such as Refs. [15–17], the light passed through the AOM only once. As a result, the different generated patterns will necessarily be propagating in different directions at the object plane of the AOM, corresponding to large relative phase gradients across the generated field distributions. A second pass through the AOM is necessary to eliminate the mode-dependent propagation direction induced by the first pass. This double-pass approach, similar to the present work, has been taken by Radwell et al., demonstrating high-speed switching between arbitrary spatial patterns of light [18]. However, this earlier work only demonstrated mode generation at a speed of 10 kHz, which is potentially attainable with fast DMDs. In contrast, we observe switching rates for mode generation of up to 500 kHz, well in excess of any existing SLM or DMD technology. Furthermore, while the modes generated in [18] were only characterized qualitatively through intensity measurements, we verify the phase structure of our generated modes quantitatively using a second hologram. In addition, we show that operating the setup in reverse allows for fast mode measurement, instead of fast mode generation. We demonstrate the projection of an unknown input state onto 3 pairs of mutually unbiased bases in a 2-dimensional Hilbert space, and use this capability to perform quantum state tomography of an unknown mode of light with a measurement rate in excess of 1 kHz and an average reconstruction fidelity of 96.9%.

2. Experimental setup

The experimental setup is shown schematically in Fig. 1. Light from a 532 nm CW laser is first coupled using an aspheric lens OBJ1 ($f=4.51\,\mathrm{mm}$) into a single-mode fiber to spatially filter the laser output and ensure consistent alignment. The light is coupled back into free space using the objective OBJ2 ($f=20\,\mathrm{mm}$), and is then sent through a telescope composed of lenses L1 and L2 ($f_1=200\,\mathrm{mm}$, $f_2=50\,\mathrm{mm}$). This telescope system ensures that the $1/e^2$ beam diameter of 0.8 mm is small enough to fit within the 2 mm active aperture of the AOM, but is also large enough to produce a small spot size in the AOM far-field, where hologram H1 is located. The light then enters the AOM (Isomet 1205C-2) driven by RF signals with frequencies equally spaced between $v_1=120\,\mathrm{MHz}$ and $v_6=70\,\mathrm{MHz}$. The RF signals are generated by an arbitrary waveform generator (AWG) that modulates a voltage-controlled oscillator (VCO), with an RF mixer used as a voltage-tunable attenuator to control the RF amplitude. The RF signal is amplified by two RF amplifiers before being sent to the AOM. The first-order diffraction from the AOM is deflected by approximately 0.15 mrad/MHz at 532 nm, corresponding to a deflection angle between 10 mrad and 18 mrad at the RF frequencies used here.

The optical system following the AOM (labeled "Mode Generation" in Fig. 1) is identical to a double pass AOM [13] used for laser frequency modulation, except for H1 taking the place of the retro-reflection mirror. After leaving the AOM, the light enters another telescope, composed of lenses L3 and L4 (with focal lengths $f_3 = 250$ mm and $f_4 = 50$ mm). This telescope acts to magnify the angular steering induced by the AOM five-fold, resulting in the full coverage of the width of H1. The light then passes through lens L5 ($f_5 = 300$ mm), which converts the different diffraction angles from the AOM to different positions on H1. Next, the beam hits a part of the static hologram H1 corresponding to a particular desired output mode. We implement H1 using an SLM (Holoeye Pluto-2, resolution 1920×1080). The photograph inset to Fig. 1 shows the appearance of H1 with the incident light impinging on it, with the six spots corresponding to the six different RF frequencies applied to the AOM. Even though all six spots appear to be present simultaneously, this is due to the exposure time of the camera being longer than the sub-ms time required for the RF frequency to switch among the six settings $v_1 \dots v_6$. In fact, only one region of H1 is illuminated at any given time. We generate the desired spatial modes in the first diffracted order from the hologram on H1, with typical diffraction efficiency of 28%.

H1 is positioned such that the beam is not exactly normal to the plane of its SLM; rather, as illustrated in Fig. 1, H1 is slightly tilted horizontally, causing the mode returning through

the AOM to be slightly displaced from the incoming beam. The returning beam is then picked off with a D-shaped mirror and sent to the "Mode Projection" stage. The light passes through another lens L6 ($f_6 = 250 \,\mathrm{mm}$), which focuses it onto a second SLM (Cambridge Correlators SDE1024, resolution 1024×768), which displays the hologram H2 corresponding to the spatial mode onto which we are projecting the input light. The light then passes through a beam sampler (Thorlabs BSF10-A) at near-normal incidence, coupling about 3.9% of the light onto a free space photodiode PD2 (Thorlabs PDA36A2), while the rest of the light is coupled to a second single mode fiber with objective OBJ3 ($f = 20 \,\mathrm{mm}$), which leads to an identical but fiber coupled photodiode PD1 (Thorlabs PDA36A2).

An arbitrary spatial mode is defined by its spatial profile, given by $A(x, y)e^{i\phi(x,y)}$, where A(x, y) is the mode amplitude and $\phi(x, y)$ is the mode phase. A hologram for generating such a mode using a phase-only SLM, denoted as $\Phi_{\text{SLM}}(x, y)$, can be found by superimposing the desired phase $\phi(x - x_0, y - y_0)$ with a linear phase grating, $k_x x + k_y y$, which separates the beam into both a first order diffraction and a zeroth-order diffraction [9]. Modulating the phase-only grating with the mode amplitude A ensures that the spatial structure of the first-order diffracted beam closely approximates the desired spatial mode. Although more sophisticated approaches exist [19], a simple choice is to use the following SLM phase pattern:

$$\Phi_{\text{SLM}}(x, y) = A(x - x_0, y - y_0) \times \left(\phi(x - x_0, y - y_0) + k_x x + k_y y \mod 2\pi\right). \tag{1}$$

The inverse grating periods (k_x, k_y) and centre positions (x_0, y_0) of the individual phase patterns on H1 were carefully optimized to correct for aberrations in the hologram and lenses L3, L4 and L5, to ensure that the light reaching H2 is precisely co-located for all generated modes. This alignment erases the information of which portion of H1 was used to produce any given spatial mode. The phase pattern given in Eq. (1) was also used to perform mode projection with H2, although in that case, the inverse grating period (k_x, k_y) and centre position (x_0, y_0) were equal for all modes.

3. Rapid mode generation

Figure 2(a) displays the static phase patterns comprising H1 used to generate 5 orthogonal orbital angular momentum (OAM) modes (Laguerre-Gauss beams with radial index p=0 and azimuthal index $l_1=-2,-1,0,1,2$), along with the mode profiles generated by this phase pattern in the far-field of H1. All of the grating patterns are displayed simultaneously in different regions of H1, with the AOM system alone being used to select the generated spatial mode. Figure 2(b) similarly shows the static phase patterns of H1 used to generate 6 states that form 3 mutually unbiased bases in the 2-D Hilbert space spanned by the $l_1=\pm 1$ states. These 6 states consist of the two $l_1=\pm 1$ OAM modes, along with horizontal, vertical, diagonal and anti-diagonal variations of the TE10 Hermite-Gauss mode. Figure 2(b) shows the simulated and imaged mode profiles generated by these phase patterns. The observed mode profiles are well aligned, with the same center position and propagation direction, which is necessary for the modes shown in Fig. 2(a) to be orthogonal and for the modes in Fig. 2(b) to form 3 mutually unbiased bases.

We characterize the quality and switching speed of mode generation by performing mode projection using H2. We fix the pattern on H2 to one that would convert a Gaussian input beam into an output beam with OAM value l_2 . Consequently, only input modes with $l_1 = -l_2$ are converted into a Gaussian beam that can couple efficiently into the fiber (SMF2). We find the coupling efficiency ϵ from the photodiode voltages V_1 and V_2 and the beam sampler splitting ratio $\eta = 3.9\%$:

$$\epsilon = \frac{1 - \eta}{\eta} \frac{V_1}{V_2} \tag{2}$$

The generation of a high-fidelity mode with OAM l_1 is confirmed by a value of ϵ close to unity when $l_1 = -l_2$, and near-zero otherwise.

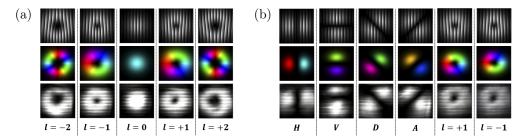


Fig. 2. Static phase patterns comprising hologram H1 are shown in the top row of images, with the middle row displaying the simulated mode profiles in the image plane (with hue indicating the phase and brightness the intensity of the field), and the bottom panel displaying the experimentally observed mode profiles generated by the AOM and H1. (a) Five OAM modes ($l_1 = -2, -1, 0, 1, 2$). (b) Six modes comprising 3 mutually unbiased bases in the 2-D Hilbert space spanned by the $l_1 = \pm 1$ states.

We step the RF frequency between 5 values, ranging from $v_1 = 120$ MHz and $v_5 = 80$ MHz, at a switching rate of up to 500 kHz, generating each of the $l_1 = -2, -1, 0, 1, 2$ OAM modes in order. Figure 3(a) shows the measured traces of the coupling efficiency ϵ into each of the corresponding output modes. As expected, ϵ is high only when $l_1 = -l_2$, indicating that the generated modes closely match the desired OAM states. The noise in ϵ is greater for times below 5 μ s, between 10 and 13 μ s, and above 19 μ s due to the lower diffraction efficiency by the AOM and H1 for those spatial modes, which results in a lower voltage V_2 on the free-space photodiode that acts to magnify any noise or fluctuation in the fiber-coupled photodiode voltage V_1 . Figure 3(b) shows a more detailed version of the gray highlighted part in Fig. 3(a). There is a 0.72 μ s delay between when the AWG ramps up the VCO voltage to output the RF frequency for $l_1 = -1$, and the time the previously generated $l_1 = 0$ mode is switched off. Following an additional delay of 1.04 μ s, the desired $l_1 = 1$ mode switches on, giving a total delay of 1.76 μ s between the moment the AWG selects mode $l_1 = 0$ and the moment this mode is first produced by the AOM and H1.

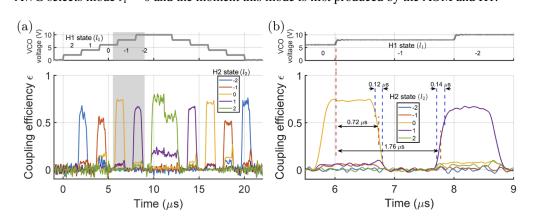


Fig. 3. Single-shot measurements of mode projection coupling efficiency for modes generated in the OAM mode basis at a rate of 500 kHz, with the corresponding VCO voltage graphs displayed above. A trace covering two full sweeps over the 5 generated modes is displayed in (a), with the gray highlighted region shown in more detail in (b).

The delays we observe are explained by the finite speed of sound through the AOM crystal, $v_s = 3.63$ km/s. At this speed, it takes sound waves $0.72 \,\mu s$ to cover the 2.6 mm distance between the piezoelectric transducer in the AOM and the first pass of the light through the AOM. The

additional delay of $1.04 \,\mu s$ is due to the $3.7 \, mm$ separation between the two passes of the light through the AOM. While these delays limit the modulation frequency in this particular experimental configuration to around 1 MHz, they are not fundamental. By aligning both passes of the light through the AOM to be within $0.5 \, mm$ of the transducer, it would be possible to reduce all delays in the system down to $140 \, ns$, permitting modulation rates of up to $5 \, MHz$.

The coupling efficiency traces shown in Fig. 3(a) contain information about the mode overlap between every pair of OAMs l_1 and l_2 , which can be expressed as the cross-talk matrix shown in Fig. 4(a). The average overlap of the generated modes with the target modes is equal to 63.6%, while the average cross-talk to each of the other modes equals 3.7%. The mode generation fidelity is limited by imperfections in the two SLMs, especially the nonlinear dependence of the optical phase shift on the gray value of the computer-generated holograms shown in the top row of Fig. 2(a). The fidelity could be improved by calibration of the SLMs used to implement the holograms [20], or through the use of binary holograms [9].

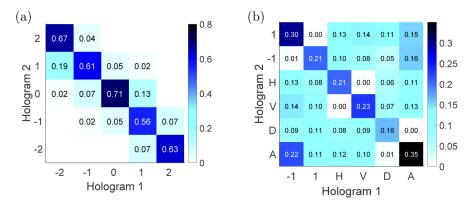


Fig. 4. Cross-talk matrices showing the overlap $|\langle \psi_2 | \psi_1 \rangle|^2$ between modes generated with the AOM and H1 and ones projected using H2. (a) OAM states shown in Fig. 2(a). (b) Six states comprising 3 mutually unbiased bases shown in Fig. 2(b).

If the mode projection on H2 was also accelerated by an AOM, the cross-talk matrix in Fig. 4(a) could be measured at a rate of 20 kHz. This rate is more than two orders of magnitude faster than the Greenwood frequency of around 60 Hz [21,22], the characteristic correlation time of turbulence-induced distortion through atmospheric channels. Therefore, our system is suitable for characterizing such channels when performing real-time adaptive optics correction, and could be used to further improve the transmission fidelity for both classical [7] and quantum [8] communication.

4. Rapid quantum state tomography

An unknown quantum state ρ in a 2-dimensional Hilbert space can reconstructed by measuring the overlap of ρ with each of six states comprising three mutually unbiased bases, analogously to characterizing a polarization state by measuring its three Stokes parameters. In the case of the space spanned by the OAM states l=1 and l=-1, these six states are the ones shown in Fig. 2(b):

$$|+1\rangle; |-1\rangle; |H, V\rangle = \frac{|1\rangle \pm |-1\rangle}{\sqrt{2}}; |D, A\rangle = \frac{|1\rangle \pm i|-1\rangle}{\sqrt{2}}.$$
 (3)

Thus, we can use the same experimental configuration as before to recover an unknown spatial mode corresponding to the hologram H2. We encode each of six states given in Eq. (3) on different regions of H1, use the AOM to switch among them, and measure the resulting coupling

efficiencies into SMF2: ϵ_{+1} , ϵ_{-1} , ϵ_{H} , ϵ_{V} , ϵ_{D} , ϵ_{A} . From these efficiencies, we determine the overlap of the unknown state ρ with the Pauli operators σ_{i} :

$$S_{x} = \operatorname{tr}(\sigma_{x}\rho) = \frac{\epsilon_{H} - \epsilon_{V}}{\epsilon_{H} + \epsilon_{V}}$$

$$S_{y} = \operatorname{tr}(\sigma_{y}\rho) = \frac{\epsilon_{D} - \epsilon_{A}}{\epsilon_{D} + \epsilon_{A}}$$

$$S_{z} = \operatorname{tr}(\sigma_{z}\rho) = \frac{\epsilon_{+1} - \epsilon_{-1}}{\epsilon_{+1} + \epsilon_{-1}}$$
(4)

which in turn implies $\rho = S_x \sigma_x + S_y \sigma_y + S_z \sigma_z$. To confirm the validity of these idealized formulas, we first realize each of the six states from Eq. (3) on H2, measuring the cross-talk matrix shown in Fig. 4(b). We see that within each pair of complementary states (i.e. each 2×2 square along the diagonal) the mode cross-talk is very low, and thus the corresponding spin projections S_i are very near to their ideal values of ± 1 .

To show that this approach is able to retrieve arbitrary modes with high fidelity, we generate a set of holograms H2 that are stored as a video file to ensure fast and consistent timing when displayed on the SLM. The first part of the video encodes a trajectory that encircles the Bloch sphere three times – once around the equator $(S_x = \cos(\omega t), S_y = \sin(\omega t), S_z = 0)$, and once each around the $\pm 45^\circ$ parallels $(S_x = \cos(\omega t)/\sqrt{2}, S_y = \sin(\omega t)/\sqrt{2}, S_z = \pm 1/\sqrt{2})$. The comparison of the theoretically expected and experimentally measured states is shown in Fig. 5(a), achieving an average fidelity of 96.8%. We then repeat the experiment with a sequence of 30 random states, as shown in Fig. 5(b), where we also see a high average fidelity of 97.1%. The fidelity is systematically lower when the quantum state generated by H2 is in a particular region of the Bloch sphere $(S_x \approx 0, S_y \approx -0.7)$ and $S_z \approx -0.7$, as can be seen for times between 1.2 s and 1.5 s in Fig. 5(a). We attribute this drop in fidelity to imperfections of the hologram H2 arising from position-dependent aberrations in the corresponding SLM. It is important to note that all the measurements were performed in a single shot, without re-playing the patterns on H2.

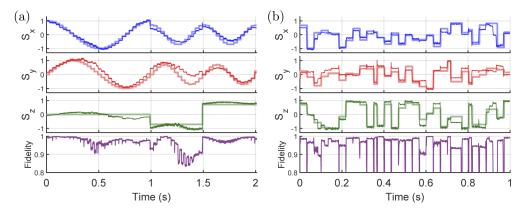


Fig. 5. Comparison of measured states (thin dark lines) against generated states (wide light lines) in a 2-D Hilbert space. The parameters S_x , S_y and S_z are the x, y and z coordinates of the state on the Bloch sphere, with the bottom panel displaying the fidelity between the generated and measured state. Panel (a) depicts a continuous trajectory wrapping around the Bloch sphere three times – once around the equator ($S_z = 0$), and once each around the $\pm 45^\circ$ parallels ($S_z = \pm 1/\sqrt{2}$), while (b) depicts a random trajectory.

For these measurements, the AOM was switching between the six modes at a rate of only 10 kHz, due to memory limitations on the oscilloscope (otherwise, the full 500 kHz switching speed demonstrated earlier could have been utilized). This means we are able to retrieve a new

estimate of the state on H2 at a rate of 1.33 kHz, much faster than the display refresh rate of the SLM (60 Hz) and fast enough to capture the transition dynamics between the different modes being generated by H2. Figure 6 illustrates one such transition near t = 0.800 s in Fig. 5(b). We can see that even though most of the transition between the initial and final modes occurs in under 1 ms, it takes about 3 ms for the transition to complete. We can also see the effect of timing fluctuations in the playback of the video on the SLM – even though we expect the mode transition to occur around t = 0.803 s, it is actually closer to t = 0.801 s. Similar signatures can be seen in Fig. 5(b). Even though we are playing back a video with a nominal frame rate of 30 Hz on an SLM with a nominal frame rate of 60 Hz, and thus expect each hologram to be displayed for a duration of 33.3 ms, we find that several frames are displayed for either 16.7 ms or 50.0 ms. We also find that occasionally the SLM produces holograms interpolating between two adjacent video frames, likely a consequence of the graphics card smoothing out the video output to the SLM for H2. While the transient behaviors we observe can be neglected in experiments with slow SLM refresh rates, they can become significant for those experiments trying to make full use of the switching speed of SLMs, such as for high-speed data transmission, turbulence compensation [7,8], or dynamical atomic trapping [23].

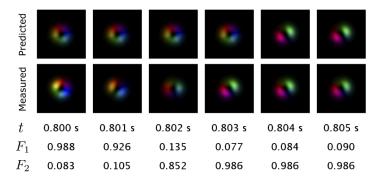


Fig. 6. Comparison of the predicted spatial modes generated by H2, assuming instantaneous updating of the displayed image (top row of images) to the spatial modes measured with the AOM and H1 (bottom row of images). F_1 indicates the fidelity between the reconstructed mode to mode expected at the start ($t = 0.800 \, \text{s}$) while F_2 is the fidelity to the mode expected at the end ($t = 0.805 \, \text{s}$). Modes and times correspond to the H2 trajectory shown in Fig. 5(b).

5. Discussion

Our measurements show that an AOM can be effectively used to multiplex different regions of a static hologram realized with an SLM, resulting in spatial mode switching rates far in excess of what can be achieved with the SLM alone. To ensure the high-fidelity generation of spatial modes, it is essential for the output modes after the second pass through the AOM to be co-located and co-propagating relative to one another, regardless of the RF frequency applied to the AOM.

That is, for each diffraction angle that the AOM applies to a beam upon its first pass, the beam must exit the AOM on its second pass in the same location, with the same transverse momentum. While a folded 4-f system we implement closely approximates this idealized situation, it is impossible to eliminate all aberrations within the setup, particularly in the position and orientation of H1 and lenses L3, L4 and L5. We were able to compensate for these aberrations by optimizing the precise position of each pattern comprising H1, as well as the period and angle of the diffraction grating for each mode.

Here, we have demonstrated the switching of 6 modes with a rate of up to 500 kHz. The switching speed could be further improved by aligning both passes of the light through the AOM closer to the transducer, which would allow rates in excess of 5 MHz. The number of multiplexed

modes could be increased by using a higher-resolution SLM, or by using two AOMs (or a 2-D AOM) to produce a grid of spots on the SLM, rather than a single row. By using both of these techniques, we estimate that up to 100 modes could be generated with a single SLM, and even thousands of modes could potentially be multiplexed by using a static hologram produced through nanofabrication. Using a nanofabricated hologram rather than an SLM would have the additional benefit of greatly increasing the damage threshold of the device, allowing its use for high-power and pulsed lasers.

This method of AOM-based hologram multiplexing could be further extended and applied in several ways. The hologram H1 could be re-written while the AOM scans the beam across the corresponding SLM, allowing for producing a high-rate stream of arbitrary modes (rather than ones picked out of a fixed library). For example, if the SLM can be updated at a rate of 100 Hz, and encode 100 different spatial modes in its different regions, the mode generation rate can be now effectively increased up to 10 kHz. Free-space turbulence could be characterized at a very high rate by using two such devices, one on the transmitter side, and the other on the receiver side, to perform quantum process tomography of the channel. A full-rank quantum process tomography for a d = 10 dimensional channel (describing arbitrary transformations of density matrices), which requires d^4 separate measurements [24], could be performed in under 10 ms with this approach. Instead of multiplexing spatial patterns on a single SLM, the AOM could also be used as the front-end to a MPLC device that converts an array of Gaussian beams into a chosen set of spatial modes, for example Laguerre-Gauss modes [11]. This combination of an AOM and MPLC would allow for high-fidelity, high-speed, and high-efficiency generation of any of the spatial modes the MPLC is capable of producing, coming close to achieving the ideal combination of speed, efficiency, scalability, and reconfigurability for devices controlling spatial modes of light.

6. Conclusion

By using an AOM in a double-pass configuration to multiplex different regions of a static hologram implemented using an SLM, we have demonstrated both the rapid generation and sorting of spatial modes of light. We switch up to 6 modes with a rate of up to 500 kHz, and apply this device to perform quantum state tomography in a 2-dimensional Hilbert space at a rate exceeding 1 kHz and an average fidelity of 96.9%. This state tomography is fast enough to directly observe the dynamics of the displayed pattern updating on another SLM. While our implementation focused on a small number of OAM spatial modes, in principle arbitrary spatial mode bases could be generated. With straightforward technical improvements, switching between 100s of modes at a rate above 1 MHz could be attained.

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Disclosures

The authors declare no conflicts of interest.

References

- 1. J. Wang, J.-Y. Yang, I. M. Fazal, N. Ahmed, Y. Yan, H. Huang, Y. Ren, Y. Yue, S. Dolinar, M. Tur, and A. E. Willner, "Terabit free-space data transmission employing orbital angular momentum multiplexing," Nat. Photonics 6(7), 488–496 (2012).
- A. E. Willner, H. Huang, Y. Yan, Y. Ren, N. Ahmed, G. Xie, C. Bao, L. Li, Y. Cao, Z. Zhao, J. Wang, M. P. J. Lavery, M. Tur, S. Ramachandran, A. F. Molisch, N. Ashrafi, and S. Ashrafi, "Optical communications using orbital angular momentum beams," Adv. Opt. Photonics 7(1), 66–106 (2015).
- G. Milione, M. P. J. Lavery, H. Huang, Y. Ren, G. Xie, T. A. Nguyen, E. Karimi, L. Marrucci, D. A. Nolan, R. R. Alfano, and A. E. Willner, "4 x 20 Gbit/s mode division multiplexing over free space using vector modes and a q-plate mode (de)multiplexer," Opt. Lett. 40(9), 1980–1983 (2015).
- Y. Ren, Z. Wang, G. Xie, L. Li, Y. Cao, C. Liu, P. Liao, Y. Yan, N. Ahmed, Z. Zhao, A. Willner, N. Ashrafi, S. Ashrafi, R. D. Linquist, R. Bock, M. Tur, A. F. Molisch, and A. E. Willner, "Free-space optical communications using orbital-angular-momentum multiplexing combined with MIMO-based spatial multiplexing," Opt. Lett. 40(18), 4210–4213 (2015).
- M. P. J. Lavery, C. Peuntinger, K. Günthner, P. Banzer, D. Elser, R. W. Boyd, M. J. Padgett, C. Marquardt, and G. Leuchs, "Free-space propagation of high-dimensional structured optical fields in an urban environment," Sci. Adv. 3(10), e1700552 (2017).
- M. A. Cox, L. Maqondo, R. Kara, G. Milione, L. Cheng, and A. Forbes, "The resilience of Hermite- and Laguerre-Gaussian modes in turbulence," J. Lightwave Technol. 37, arXiv:1901.07203 (2019).
- 7. Y. Ren, G. Xie, H. Huang, N. Ahmed, Y. Yan, L. Li, C. Bao, M. P. J. Lavery, M. Tur, M. A. Neifeld, R. W. Boyd, J. H. Shapiro, and A. E. Willner, "Adaptive-optics-based simultaneous pre- and post-turbulence compensation of multiple orbital-angular-momentum beams in a bidirectional free-space optical link," Optica 1(6), 376–382 (2014).
- 8. J. Zhao, Y. Zhou, B. Braverman, C. Liu, K. Pang, N. K. Steinhoff, G. A. Tyler, A. E. Willner, and R. W. Boyd, "Performance of real-time adaptive optics compensation in a turbulent channel with high-dimensional spatial-mode encoding," Opt. Express 28(10), 15376–15391 (2020).
- A. Forbes, A. Dudley, and M. McLaren, "Creation and detection of optical modes with spatial light modulators," Adv. Opt. Photonics 8(2), 200–227 (2016).
- A. Sit, F. Bouchard, R. Fickler, J. Gagnon-Bischoff, H. Larocque, K. Heshami, D. Elser, C. Peuntinger, K. Günthner, B. Heim, C. Marquardt, G. Leuchs, R. W. Boyd, and E. Karimi, "High-dimensional intracity quantum cryptography with structured photons," Optica 4(9), 1006–1010 (2017).
- 11. N. K. Fontaine, R. Ryf, H. Chen, D. T. Neilson, K. Kim, and J. Carpenter, "Laguerre-Gaussian mode sorter," Nat. Commun. 10(1), 1865 (2019).
- V. V. Nikulin, R. M. Khandekar, and J. Sofka, "Agile acousto-optic tracking system for free-space optical communications," Opt. Eng. 47(6), 064301 (2008).
- E. A. Donley, T. P. Heavner, F. Levi, M. O. Tataw, and S. R. Jefferts, "Double-pass acousto-optic modulator system," Rev. Sci. Instrum. 76(6), 063112 (2005).
- 14. S. I. Ksouri, M. Mattern, J. Kahler, A. Aumann, G. Zyla, and A. Ostendorf, "Holographic optical tweezers: microassembling of shape-complementary 2PP building blocks," in *Optical Trapping and Optical Micromanipulation XI*, vol. 9164 K. Dholakia and G. C. Spalding, eds., International Society for Optics and Photonics (SPIE, 2014), pp. 451–455.
- 15. P. St-Hilaire, S. A. Benton, M. E. Lucente, J. S. Underkoffler, and H. Yoshikawa, "Real-time holographic display: improvements using a multichannel acousto-optic modulator and holographic optical elements," J. Opt. Soc. Am. (1901)
- M. Mestre, B. Viaris de Lesegno, R. Farcy, L. Pruvost, J. Bourderionnet, A. Delboulbe, B. Loiseaux, and D. Dolfi,
 "Fast reconfigurable and transient-less holographic beam-shaping realized by a aom-slm device," Eur. Phys. J.: Appl.
 Phys. 40(3), 269–274 (2007).
- M. Haney and D. Psaltis, "Real-time programmable acoustooptic synthetic aperture radar processor," Appl. Opt. 27(9), 1786–1796 (1988).
- N. Radwell, D. Brickus, T. W. Clark, and S. Franke-Arnold, "High speed switching between arbitrary spatial light profiles," Opt. Express 22(11), 12845–12852 (2014).
- E. Bolduc, N. Bent, E. Santamato, E. Karimi, and R. W. Boyd, "Exact solution to simultaneous intensity and phase encryption with a single phase-only hologram," Opt. Lett. 38(18), 3546–3549 (2013).
- X. Xun and R. W. Cohn, "Phase calibration of spatially nonuniform spatial light modulators," Appl. Opt. 43(35), 6400–6406 (2004).
- 21. D. P. Greenwood, "Bandwidth specification for adaptive optics systems*," J. Opt. Soc. Am. 67(3), 390–393 (1977).
- 22. G. A. Tyler, "Bandwidth considerations for tracking through turbulence," J. Opt. Soc. Am. A 11(1), 358–367 (1994).
- D. Stuart and A. Kuhn, "Single-atom trapping and transport in DMD-controlled optical tweezers," New J. Phys. 20(2), 023013 (2018).
- M. Mohseni, A. T. Rezakhani, and D. A. Lidar, "Quantum-process tomography: Resource analysis of different strategies," Phys. Rev. A 77(3), 032322 (2008).